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In this paper, we demonstrate that the superposition of two vortex beams with controlled topological charges can be realized by integrating two holographic plates with blazed grating. First, the holographic plate with blazed grating was designed and fabricated by laser direct writing for generating well-separated vortex beam. Then, the relationship between the periods of blazed grating and the discrete angles of vortex beams was systematically investigated. Finally, through setting the discrete angle and different revolving direction of the holographic plates, the composite fork-shaped field was realized by the superposition of two vortex beams in a particular position. The topological charges of composite fork-shaped field \( l = 1, 0, 3, \) and 4) depend on the topological charges of compositional vortex beams, which are well agreed with the theoretical simulation. The method opens up a wide range of opportunities and possibilities for applying in optical communication, optical manipulations, and photonic integrated circuits. Published by AIP Publishing. [http://dx.doi.org/10.1063/1.4997590]

Optical vortices with helical phase wave-fronts carrying orbital angular momentum (OAM) have a phase winding factor described by \( \text{exp}(i\phi) \), where \( \phi \) is the azimuthal angle, \( l \) is the topological charge of orbital angular momentum of \( \hbar \) per photon, and the positive or negative of topological charges represents different revolving direction of the phase fronts around the beam axis. ¹ Optical vortex has shown great potential in modern optics and photonics due to their unprecedented promising applications in optical communication, ² and optical manipulation. ³ Researchers obtained vortex beam based on a few optical components such as spiral phase plates, ⁴ q-plates, ⁵ whispering gallery modes resonator, ⁶–⁸ spatial light modulators (SLM), ⁹ metasurfaces, ¹⁰–¹² and nano-fabricated holograms. ¹³,¹⁴ In addition, when a vortex beam is superimposed with another one, the phase distribution of the composite vortex is dependent on the compositional vortex beams, and the superposed OAM states would also change due to the superposition of different vortex beams. ¹⁵ The superposed OAM beams are possible to provide arbitrary OAM states for optical applications by increasing the number of compositional OAM modes in the superposition. Recently, Wang et al. ¹⁶ adopted a variable amplitude splitter and an OAM emitter were adopted generate the superposition of optical vortex beams. ⁷ Moreover, a computer-generated hologram was utilized to produce the high-order superposed OAM modes for spinning object detection. ⁹ But these methods significantly increase the complexity and volume of experimental systems. Therefore, a simple, efficient, and compact approach to achieve the superposition of two vortex beams is highly desirable.

In our work, we propose a compact strategy—two holographic plates with blazed grating (HPBGs) to realize the superposition of two vortex beams with controlled topological charges. Single HPBG (\( \sim 60 \mu \text{m} \) size) was fabricated by direct laser writing, which can simultaneously generate and separate the first order optical vortices. Two HPGs were used to generate superposed vortex beams by setting the discrete angle and revolving direction of every HPBG. Moreover, the relation between the topological charges of superposed vortex beams and compositional vortex beams was studied. The integrated HPGs can be applied in optical tweezers, ¹⁵ optical communication, ¹⁶ and photonic integrated circuits. ¹²,¹⁷,¹⁸ A forked diffraction grating (the topological charges \( l = 1 \)) was created by the phase distribution of the desired optical component plus a linear phase ramp, ¹⁹ the whole structure consists of blazed grating and substrate [Figs. 1(a) and 1(b)]. The blazed grating was designed by using periodic gray value based on diffraction grating, which illustrates the blazed grating has grooves with a sawtooth-shaped profile. The thickness of sawtooth is defined as \( h = \frac{\lambda}{n_0} \) with \( \lambda \) the wavelength of incident light, \( n \) (\( \sim 1.504 \)) the refractive index of HPBG, and \( n_0 \) (\( \sim 1 \)) the refractive index of air. \( d \) represents the grating period. The HPBG was fabricated by femtosecond-laser direct laser writing on photoresist (SZ2080, provided by FORTH, Greece). ²⁰ Typical scanning electron microscopy (SEM) image of polymerized HPBG with a 60 \( \mu \text{m} \) diameter is shown in Fig. 1(c), which illustrates the fabricated structure is consistent well with the designed model. The measured thickness of sawtooth is 1.02 \( \mu \text{m} \) [The inset of Fig. 1(c)], which is in good agreement with theoretical value of 1.05 \( \mu \text{m} \). The sample was characterized by using a simple optical system [Fig. 1(d)]. The light
from the 532 nm wavelength laser was passed through a pin-
hole ($P1$) and objective lens $L1$ (numerical aperture $NA = 0.6$),
and then focused on the sample (about 72% transmission effi-
ciency). The generated vortex beam was collimated by objec-
tive lens $L2$ ($NA = 0.4$), and incident on a charge coupled
device (CCD) camera.

A simple single beam original interferometric technique
was adopted to characterize the phase singularity of the gener-
ated vortex beams, and the size of pinhole was adjusted to
realize the interference of the vortex beam. Considering that
the focal plane of the incident focused Gaussian beam is
located at the Fresnel diffraction region, we can observe the
transmitted diffraction patterns from HPBGs. The vortex
beam diffracted into the $m$-th order acquires a singular phase
with topological charge $q = m/C1l$, and here, we will concen-
trate on the case of $m = 1$. Schematic of HPBG with shifted vortex
beam is shown in Fig. 2(a), from which we can observe the
generated vortex beam shift outside the laser spot without the
reference beam. As shown in Figs. 2(b)–2(e), with the topo-
logical charge increasing, the central dark region becomes
bigger and the donut ring becomes thinner. Then, we adjust
the pinhole a little bigger so that the generated vortex beam
interferes with the surrounding laser spot [Fig. 2(f)]. In Figs.
2(g)–2(k), we can find the central fringe of the interference
pattern is obviously divided into $l$ forks. The intensity of
Gaussian beam peaks at the center, and it gradually weakens
from center to edge, but the fringe contrast of interference is
smallest at the center. Therefore, we can see that the central
interference patterns are blurring, which are in good agree-
ment with simulations [Figs. 2(g′)–(k′)].

To obtain a greater shifted distance from the center of
HPBG, we studied the relationship between the periods of
blazed grating and the discrete angles of vortex beams. The
blazed grating usually concentrates as much of the incident
light as possibly into only the first order by designing
sawtooth-shaped profile. The shifted vortex beam depends
on the sawtooth-shaped profile, which has two important
parameters: the thickness and the grating period. According
to the gray value change of designed hologram and a 60 μm
diameter HPBG, we theoretically calculate the grating period
$d_i$, which can be expressed as

$$d_i = \frac{51}{i\pi},$$

where $i = 2, 3, 4, \text{ and } 5$ (the generated vortex beam need to
shift outside the laser spot, $i > 1$). According to Eq. (1),
we can obtain $d_2 = 8.12 \mu m$, $d_3 = 5.41 \mu m$, $d_4 = 4.06 \mu m$, $d_5 = 3.25 \mu m$, and the theoretical values are consistent with the
experimental results [Fig. 1(c)]. The diffracted beams propa-
gate at the discrete angles, which can be expressed as

$$\theta_i = \frac{\lambda}{d_i},$$

FIG. 1. (a) A forked diffraction grating with topological charge $l = 1$ created
by the phase distribution of the desired optical component plus a linear
phase ramp. (b) The ideal three dimensional HPBG with a sawtooth-shaped
profile consisting of blazed grating and substrate. The blazed grating was
designed by using periodic gray value based on diffraction grating. (c) SEM
images of a 60 μm diameter. Inset: thickness profile extracted from the part
of structure. $h = 1.02 \mu m$, $d = 4.19 \mu m$. (d) Schematic illustration of the
optical performances detection setup.

FIG. 2. (a) Schematic illustration of
HPBG with shifted vortex beam, the
generated vortex beam shift outside
the laser spot without the reference
beam. (b)–(e) Experimental and theo-
retical far field intensity patterns of the
generated vortex beam with topologi-
cal charge $l = -2, -1, 1, \text{ and } 2$. (f) The
generated vortex beam interferes with
the surrounding laser spot. (g)–(k)
Experimental and theoretical interfer-
ence patterns of the generated vortex
beam and the reference beam, the cen-
tral fringe of the interference pattern is
obviously divided into $l$ forks. The the-
oretical patterns match well with the
observed ones.
where \( \lambda \) is the wavelength of incident light. So, the different grating periods can produce different discrete angles, and the vortex beams with different discrete angles correspond to different shifted distances. For applications requiring isolated vortex beams, it is necessary to use holograms with small grating periods. Different transmission HPBGs with grating periods of \( d_2, d_3, d_4 \), and \( d_5 \) (the topological charge \( l = 2 \) and 60 \( \mu \)m diameter) were fabricated, as shown in Figs. 3(a)–3(d). The HPBG with different grating periods can produce different shifting distances, and the smaller the grating periods, the greater the shifting distances. The shaded part of the red circle is the location of the structure, and the generated vortex beam can be shifted out of the laser spot. According to the shifting distance, we can experimentally calculate the discrete angles, which can be expressed as

\[
\delta_x = \frac{x_i}{f}, \tag{3}
\]

where \( x_i \) is the shifted distances corresponding to different grating periods, and \( f \) is the distance between the sample and the observation screen [the inset of Fig. 3(e)]. After measuring \( x_i \) and \( f \), discrete angles were obtained, which show a good agreement with theoretical calculations [Fig. 3(e)].

The \( m \)-th diffraction order can be divided into positive and negative diffraction orders. These negative diffraction orders propagating to one side of the central order beam have quantized OAM that is antiparallel to the propagation direction, and vice versa for positive diffraction orders.1 We defined that positive diffraction orders propagate to the right side of the central order beam, so the superposition of two vortex beams is the superposition of the positive diffraction order of vortex beam and the negative diffraction order of another vortex beam (here we will concentrate on the case \( m = +1, -1 \)). The superposed light field can be considered a kind of composite fork-shaped field. The topological charges of composite fork-shaped field are equal to the sum of two topological charges, which can be expressed as

\[
l = (l_1) + (-l_2), \tag{4}
\]

where \( "+" \) and \( "-" \) represent the positive and negative diffraction orders of vortex beams, respectively. Further, when two vortex beams with different phase distribution are appropriately weighted to give the different intensity distributions, the relative phases of these two modes can be interactional in composite field so that they interfere destructively at their common focus to give forked intensity distribution. Two vortex beams with topological charges \( l_1 = 2 \) and \( l_2 = 2 \) can be superposed. Figure 4(a) shows a SEM image of 4.06 \( \mu \)m-period HPBGs with different revolving directions, in which the left one is the counterclockwise rotation of 60° and the right one is counterclockwise rotation of 120°. A schematic illustration of superposition of two vortex beams is shown in Fig. 4(b). Through setting the discrete angle and different revolving direction of the holographic plates, those two vortex beams can be superposed in a fixed space diffraction distance, and the CCD is placed at the designed diffraction distance and detect the superposition of two OAM beams.

The topological charge of composite fork-shaped field \( l = 0 \), Fig. 4(e) is created by the superposition of the positive diffraction order of vortex beam with topological charge \( l_1 = 2 \) and the negative diffraction order of vortex beam with topological charge \( l_2 = 2 \). The superposed patterns of other different topological charges \( [l(l_1 = 1, l_2 = -2) = -1, l(l_1 = 1, l_2 = -2) = 3, \text{and } l(l_1 = 2, l_2 = -2) = 4] \) are shown in Figs. 4(c), 4(d), and 4(f), which are well agreed with the theoretical result of composite fork-shaped field [Figs. 4(g)–4(j)]. The phase distributions of composite fork-shaped field are shown in Figs. 4(k)–4(n). The composite OAM states are determined by component vortex beams with different topological charges, while the topological charges can only be changed by switching HPBG with different topological charges. In order to obtain larger OAM, we can simply integrate two HPBGs with two smaller the topological charges. Here, our proposed approach is very robust, since it not only overcomes complex experimental setup problems of conventional ways for producing OAM superposition, such as Segnac interferometer,22 consisting of an OAM beam generator, beam splitters, Dove prism, and mirrors, but also efficiently

FIG. 3. (a)–(d) Microscope patterns of HPBG with different grating periods. The smaller the grating periods, the greater the shifting distances of the generated vortex beams. The shaded part of the red circle is the location of the structure, and the large red circle is the location of a laser spot. (e) The theoretical \( \theta \) (the blue line) compares to experimental \( \theta' \) (the red dot). The inset shows that the generated vortex beam shift the center of HPBG.
generates composite OAM beams with controlled topological charges.

In conclusion, we experimentally and theoretically demonstrate that the superposition of two vortex beams can be achieved by integrating HPBGs with different revolving direction and setting the discrete angle. The smaller-size (~60 µm) HPBG with controlled topological charges fabricated by high fidelity direct laser polymerization can be used simultaneously to generate and separate vortex beam. The relationship between the blazed grating with different grating periods and its discrete angles was also investigated. In addition, we have demonstrated that the superposition of two vortex beams is the superposition of the positive diffraction order of vortex beam and the negative diffraction order of another vortex beam, and the OAM states of composite fork-shaped field are determined by the topological charges of compositional vortex beams. Due to the simplicity of our design, this method not only overcomes complex experimental setup problems of conventional ways, but also efficiently generates composite OAM beams with controlled topological charges.

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FIG. 4. (a) A SEM image of integrated HPBGs with different revolving direction, and the diameter and grating periods of single structure are 40 µm and 4.06 µm. (b) Schematic illustration of superposition of two vortex beams. (c)–(f) The superposed patterns of the generated vortex beams with different topological charges. The topological charges of fork-shaped field (l = −1, 0, 3, and 4) is equal to the sum of two topological charges. (g)–(j) Theoretical results correspond to (c)–(f). (k)–(n) The phase distributions of the fork-shaped field. The theoretical patterns match well with the observed ones.